

ADOPTION NOTICE

National Electrical Manufacturers Association (NEMA) Standard NEMA WC 56, "*3.0 kHz Insulation Continuity Proof Testing of Hook-up Wire*", was adopted on 11 August 2000 for use by the Department of Defense (DoD). Proposed changes by DoD activities must be submitted to the DoD Adopting Activity: Defense Logistics Agency, Defense Supply Center, Columbus, ATTN: DSCC-VAI, P.O. Box 3990, Columbus, OH 43216-5000. DoD activities may obtain copies of this standard from Document Automation and Production Service, Building 4/D, 700 Robbins Avenue, Philadelphia, PA 19111-5094. The private sector and other Government agencies may purchase the document from the National Electrical Manufacturers Association, 1300 North 17th Street, Suite 1847, Rosslyn, VA 22209.

CONCLUDING MATERIAL

Custodians:

Navy - SH

Air Force - 11

DLA - CC

Adopting Activity:

DLA - CC

(Project 6145-2257)

Review activity:

Navy - AS

NEMA STANDARDS PUBLICATION NO. WC 56

nema

**3.0 kHz
Insulation
Continuity
Proof
Testing
of Wire
and Cable**



NATIONAL ELECTRICAL MANUFACTURERS ASSOCIATION



2101 L STREET, N.W., WASHINGTON, D.C. 20037

NEMA Standards Publication No. WC 56-1986 (R 1993)
3.0 kHz INSULATION CONTINUITY PROOF TESTING OF WIRE AND CABLE
Revision 1, February 15, 1994

Published by

National Electrical Manufacturers Association
2101 L Street, N.W.
Washington, DC 20037

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Foreword

This Standards Publication has been prepared to delineate the basic requirements for sparktesting apparatus utilizing a 3 kHz nominal frequency. It is intended as a substitute or an alternative to conventional sparktesting at an industrial frequency.

The use of an elevated frequency will allow a reduction in the electrode length while exposing the wire or cable to a suitable number of wave crests.

Performance criteria have been included which will stipulate minimum sensitivities for the equipment. Underwriters Laboratories has recognized 3 kHz sparktest for testing of wire or cable. The NEMA High Performance Wire and Cable Section prepared this test procedure.

Comments or proposed revisions are welcomed and should be submitted to:

Vice-President, Engineering
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Washington, D.C. 20037

Scope

This standard covers a general procedure for continuous voltage proof testing of wire and cable. It is intended to apply primarily to the final inspection of wire or cable for the purpose of finding and eliminating defects prior to shipment or before use. The method can also be used to eliminate defects at an early stage of manufacturing, i.e., for wire or cable to be used in multiconductor cables or jacketed constructions.

Because of possible damage in handling, damage caused by repeated testings, and variations in test parameters, comparison between producer's and consumer's test results are not significant.

Section 1 TEST EQUIPMENT

1.1 ELECTRODE

The electrode shall be of a bead chain construction (see Figure 1-1) that will give intimate metallic contact with practically all of the wire insulation surface.

The chain shall be suspended in a U or V-shaped trough having a width approximately $1\frac{1}{2}$ inches (38 mm) greater than the diameter of the larger size of wire that is tested.

The chain shall have a length appreciably greater than the depth of the enclosure so that the beads will droop below the wire under test.

The electrode shall consist of an array of $1/16$ inch (1.59 mm) diameter stainless steel bead chains suspended approximately 0.08 inch (2.03 mm) apart, perpendicular to the wire line and spaced approximately 0.10 inch (2.54 mm) apart along the wire line.

1.1.1 Electrode Length

The electrode length shall be chosen so that, at the speed being used, the wire shall be subjected to no less than a total of six positive and negative crests of the supply voltage (the equivalent of three complete cycles nor more than 1200 positive or negative wave crests (600 complete cycles) at any given cross section.

1.1.2 Use of Electrode

Only one electrode shall be connected to the power supply transformer.

The electrode shall be kept free of water and foreign matter; it shall be provided with an earth grounded metal screen or an equivalent guard to provide protection for the operating personnel.

Broken chains shall be replaced as required.

1.2 VOLTAGE SHAPE

The applied voltage shall be essentially sinusoidal. The crest factor of the voltage shall be no less than 1.35 nor more than 1.48 under any load condition (see 2.3).

1.3 VOLTAGE FREQUENCY

The frequency shall be 2.5 ± 1.0 kHz under any load condition.

The most desirable frequency range is 3 ± 0.5 kHz. There are wire and cable constructions which will cause the frequency to drop below 2.5 kHz. Under no conditions shall the frequency be allowed to go below 1.5 kHz. Line speeds should be adjusted at low frequencies. Use 2.1.3.1 to calculate the speed.

If equipment with multiple load or frequency settings is used, it shall contain a frequency meter or tripping device which will render the unit non-operational when the frequency does not fall within the specified range.

1.4 VOLTMETER

The voltmeter measuring the rms voltage shall be capable of operating accurately up to 4 kHz, shall be connected directly to the measuring circuit, and shall continually indicate the electrode potential.

The full scale meter reading shall not be greater than 15 kV rms.

The meter accuracy shall be such that, when the voltage is adjusted to any specified value by a calibrating voltmeter, the actual electrode value will be within ± 2 percent of full scale.

1.5 REGULATION

The maximum current which the equipment can deliver to a purely capacitive load shall be no less than 40.0 milliamperes. The maximum current which can be delivered to purely resistive load shall be no greater than 4.0 milliamperes. The voltage at the test electrode shall not change more than 5 percent between no load and full load conditions when the load consists of a capacitance passing a current of 10.0 milliamperes in parallel with a resistance passing a current of 1.0 milliampere.

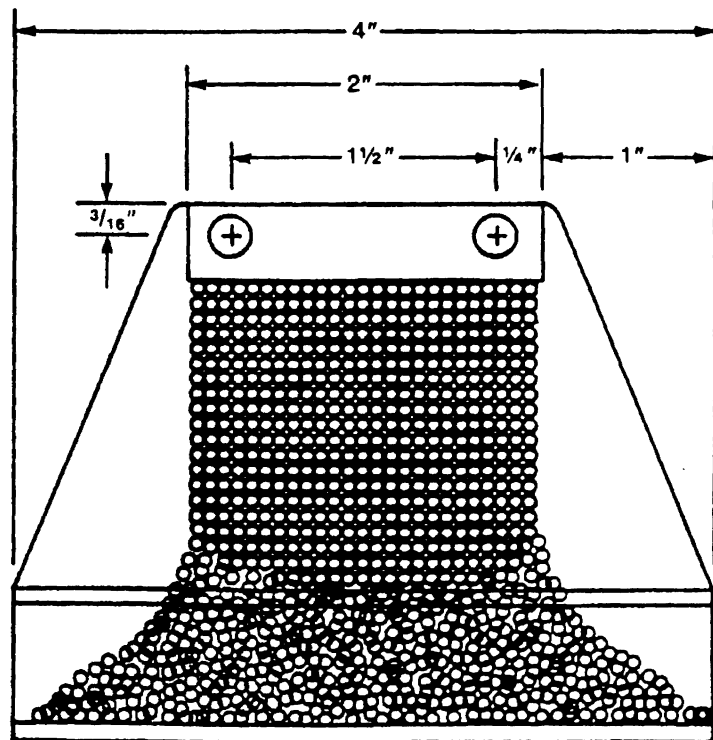
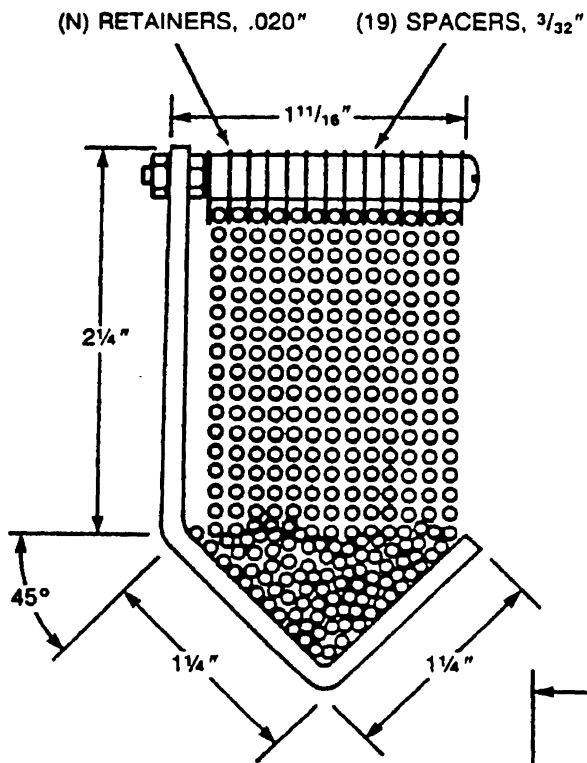
1.6 FAILURE DETECTION CIRCUIT

There shall be a fault indicating circuit which shall give a visible or audible indication of a dielectric failure. The system shall be sufficiently sensitive so that a fault is indicated at any voltage above 2 kV when the electrode is arced to ground through a needle spark gap in series with a test network, for a duration of 1 millisecond (see Figure 1-2).

The spark gap shall consist of a metal plate and a needle point, and the distance between them shall be maintained at $.010$ inch $\pm .002$ inch ($.25$ mm $\pm .05$ mm). A suitable type of needle is shown in Figure 1-3, or equivalent. The 50 picofarad (pf) capacitor shall be of the high voltage type (15 kV rms) with polyethylene insulation, or suitable equivalent.

After a fault occurs, the equipment shall come back to full sensitivity and full potential within 40 milliseconds.

Equipment used for proof testing without stopping mechanism shall have a response time such that every segment of the wire will be subjected to the full test potential at full sensitivity and fault registering capability for at least three complete cycles.



*Note: All dimensions in inches.

Figure 1-1
TYPICAL BEAD CHAIN ARRANGEMENT

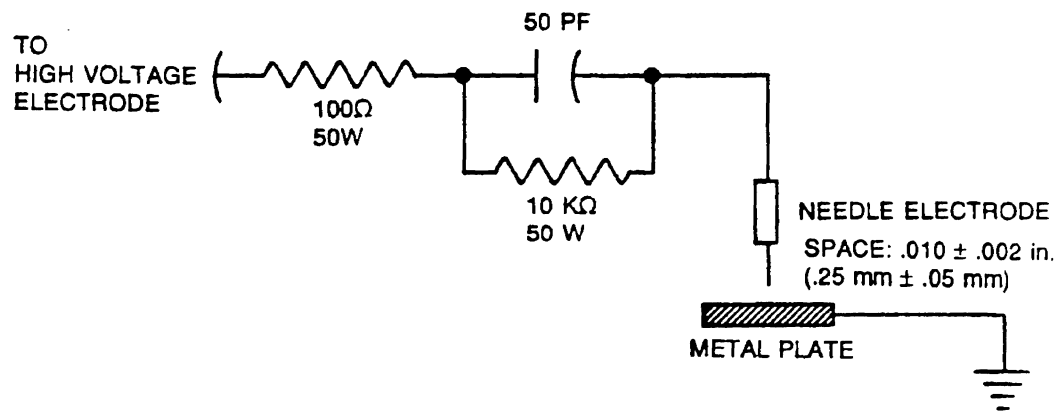


Figure 1-2
TYPICAL ARRANGEMENT FOR SENSITIVITY MEASUREMENT

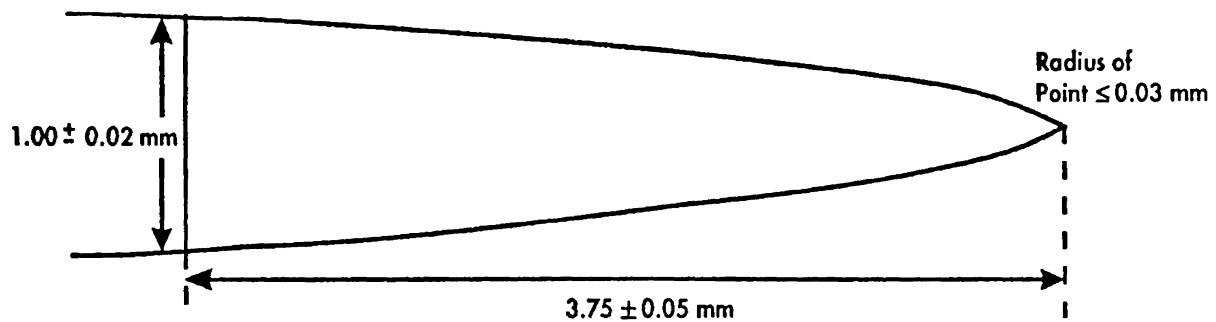


Figure 1-3
SUITABLE NEEDLE POINT

There shall be no indication of a fault when the electrode is shorted to ground through a 2 megohm resistor at a voltage of 2 kV for a period of 2 seconds.

1.7 SAFETY OF EQUIPMENT AND SAFE USE OF EQUIPMENT

Any equipment built or purchased for performance of this test shall comply with applicable electrical safety codes, and shall be used in accordance with the manufacturer's instructions for safe use.

Section 2 TEST PROCEDURE

2.1 SET-UP

The insulated wire or cable shall be threaded through the electrode head and the conductor grounded at one or both ends. With the electrode head energized to the specified voltage, the wire shall pass from the payoff spool through the electrode and on to the takeup spool.

2.1.1 Voltage

The voltage shall be adjusted with the wire or cable in the electrode. The equipment shall not be used if any noticeable voltage drop occurs when the wire starts moving through the electrode at any selected speed.

2.1.1.1 MAXIMUM VOLTAGE

Loading of the equipment beyond its power supply capabilities may result in malfunctioning or erroneous indications. The maximum allowable voltage may therefore have to be restricted due to capacitive loads. It may be calculated based on the minimum current necessary to trigger the detection circuit (40 milliamperes per paragraph 1.5) divided by $2\pi F$ (where F is frequency) and the capacitance of the wire in the electrode. For purposes of this determination, the maximum allowable frequency of 3.5 kHz should be used, so that maximum voltage is determined as follows:

$$V_{\max} = \frac{1.82(10)^6}{C} \quad (\text{Volts})$$

Where:

V = Volts

C = Capacitance in Picofarads (pf)

Modern high performance insulation systems may not require any such determination for the resistive component to calculate the maximum allowable voltage; for lossy dielectrics, however, a maximum allowable voltage should also be calculated for the resistive component of the load current.

2.1.2 Frequency

Equipment with multiple settings shall be adjusted such that the test frequency will be 2.5 ± 1.0 kHz.

2.1.3 Line speed

The rate of speed, as a function of electrode length, shall be controlled by the requirements of 1.1.1.

2.1.3.1 MAXIMUM

The maximum acceptable line speed in feet per minute (fpm) shall be determined as follows:

$\text{fpm} = 5/3 \times \text{Frequency (Hz)} \times \text{Electrode Length (in.)}$, when calculated for the lowest allowable frequency of 1.50 kHz. Therefore $\text{fpm}_{(\max)} = 2500 \times \text{Electrode Length (in.)}$.

Similarly, for metric units, line speed in meters per minute shall be determined as follows:

$\text{Meters per minute} = 1/50 \times \text{Frequency (Hz)} \times \text{Electrode Length (mm)}$.

Therefore:

$\text{Meters per minute}_{(\max)} = 30 \times \text{Electrode Length (mm) at 1.50 kHz}$.

2.1.3.2 MINIMUM

The minimum acceptable line speed shall be determined based on the maximum frequency of 3.50 kHz as follows:

Where Max. frequency = 3.50 kHz, Max. No. of cycles per given area = 600, and for 1 inch of electrode length at 3.50 kHz/600 cycles, then $\text{fpm}_{(\min)} = 5.833 \text{ inch/second} \times 60 \text{ seconds/minute} \times 1 \text{ foot/12 inches} = 29.2 \times \text{Electrode Length (in.)}$.

Similarly, for metric units:

$\text{Meters per minute}_{(\min)} = 29.2 \text{ feet/minute/inch} \times .305 \text{ meter/foot} \times .0394 \text{ millimeter/1 inch} = .35 \times \text{Electrode Length (mm)}$.

2.2 FAULT IDENTIFICATION

If any dielectric failures occur, they shall be cut out or suitably identified for subsequent removal, together with at least 2 inches (50.8 mm) of wire on each side of the fault. The equipment shall be wired to automatically de-energize the high voltage when the wire is stopped. During the string-up of a new length, every attempt shall be made to expose the entire length, including ends, to the specified voltage. Any ends not tested shall be clearly marked and removed subsequent to this test.

2.3 CALIBRATION AND CREST FACTOR

The instrument voltmeter and waveform shall be checked for compliance with this standard at 25, 50, 75, and 100 percent of each intended operating voltage scale by means of a calibrated electrostatic voltmeter with peak detecting attachment. The voltmeter without attachment shall be used to measure the rms voltage; the crest voltage shall be measured with the peak detecting attachment and the same electrostatic voltmeter shall be used for measurement of the rms value. The ratio of the crest value to the rms value constitutes the form factor which must fall

within the limits specified in 1.2, under no load and full load conditions.

2.4 VENTILATION OF WORK AREA

Provisions for ventilation may have to be made when using the equipment described in this standard in a closed

room, in order to remove any excess ozone which may be formed during the testing, particularly at higher voltages.